

125W STEREO / 250W MONO PurePath™ HD ANALOG-INPUT POWER STAGE

Check for Samples: [TAS5611](#)

FEATURES

- PurePath™ HD Enabled Integrated Feedback Provides:
 - Signal Bandwidth up to 80kHz for High Frequency Content From HD Sources
 - Ultralow 0.03% THD at 1W into 4Ω
 - Flat THD at all Frequencies for Natural Sound
 - 80dB PSRR (BTL, No Input Signal)
 - >100dB (A weighted) SNR
 - Click and Pop Free Startup
- Pin compatible with TAS5630, TAS5615 and TAS5613
- Multiple Configurations Possible on the Same PCB With Stuffing Options:
 - Mono Parallel Bridge Tied Load (PBTL)
 - Stereo Bridge Tied Load (BTL)
 - 2.1 Single Ended Stereo Pair and Bridge Tied Load Subwoofer
- Total Output Power at 10%THD+N
 - 250W in Mono PBTL Configuration into 2Ω
 - 125W per Channel in Stereo BTL Configuration into 4Ω
- Total Output Power in BTL configuration at 1%THD+N
 - 130W Stereo into 3Ω
 - 105W Stereo into 4Ω
 - 70W Stereo into 6Ω
 - 55W Stereo into 8Ω
- >90% Efficient Power Stage With 60-mΩ Output MOSFETs
- Self-Protection Design (Including Undervoltage, Overtemperature, Clipping, and Short-Circuit Protection) With Error Reporting
- EMI Compliant When Used With Recommended System Design
- Two Thermally Enhanced Package Options:
 - PHD (64-Pin QFP)
 - DKD (44-Pin PSOP3)

APPLICATIONS

- Home Theater Systems
- AV Receivers
- DVD/Blu-ray Receivers
- Mini Combo System
- Active Speakers and Subwoofers

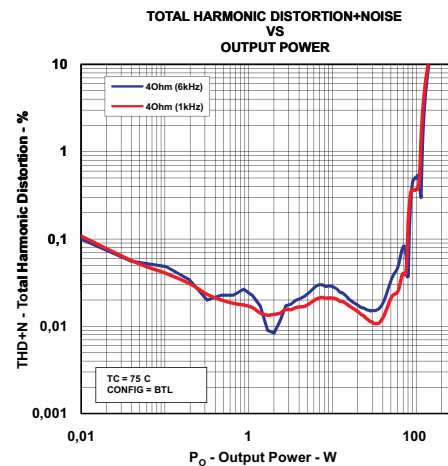
DESCRIPTION

The TAS5611 is a high performance analog input Class D amplifier with integrated closed loop feedback technology (known as PurePath™ HD) with the ability to drive up to 125W ⁽¹⁾ Stereo into 4 to 8 Ω Speakers from a single 32.5V supply.

PurePath™ HD technology enables traditional AB-Amplifier performance (<0.03% THD) levels while providing the power efficiency of traditional class D amplifiers.

Unlike traditional Class D amplifiers, the distortion curve only increases once the output levels move into clipping.

PurePath™ HD technology enables lower idle losses making the device even more efficient.



- (1) Achievable output power levels are dependent on the thermal configuration of the target application. A high performance thermal interface material between the package exposed heatslug and the heat sink should be used to achieve high output power levels.



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These devices have limited built-in ESD protection. The leads should be shorted together or the device placed in conductive foam during storage or handling to prevent electrostatic damage to the MOS gates.

DEVICE INFORMATION

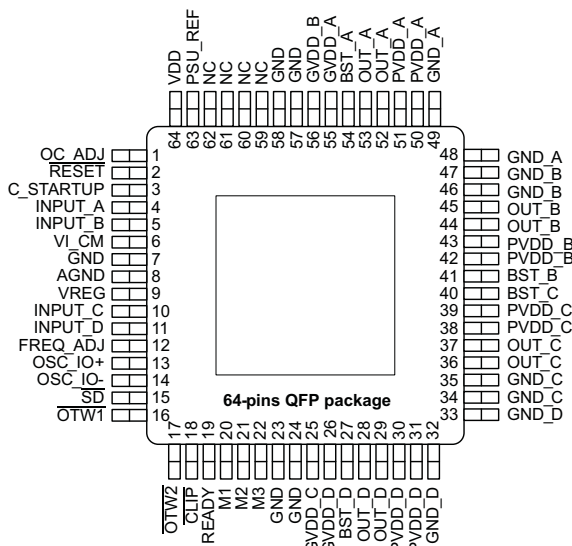
Terminal Assignment

The TAS5611 is available in two thermally enhanced packages:

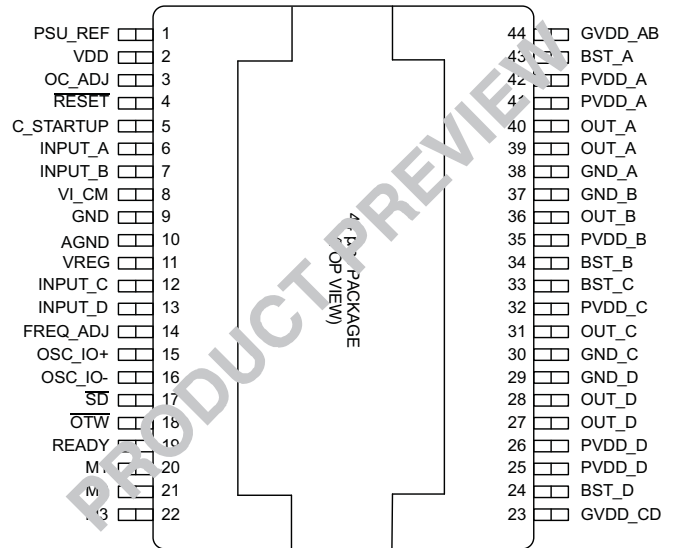
- 64-Pin QFP (PHD) Power Package
- 44-Pin PSOP3 package (DKD)

The package types contain heat slugs that are located on the top side of the device for convenient thermal coupling to the heat sink.

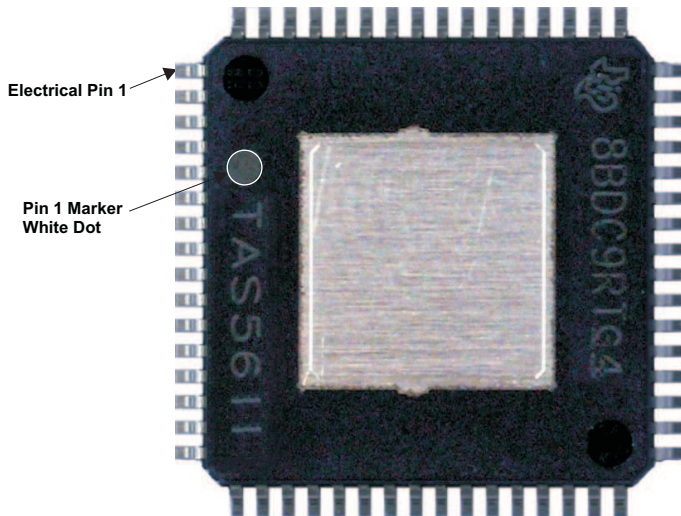
PHD PACKAGE
(TOP VIEW)



DKD PACKAGE
(TOP VIEW)



PIN ONE LOCATION PHD PACKAGE



MODE SELECTION PINS

MODE PINS			ANALOG INPUT	OUTPUT CONFIGURATION	DESCRIPTION		
M3	M2	M1					
0	0	0	Differential	2 × BTL	AD mode		
0	0	1	—	—	Reserved		
0	1	0	Differential	2 × BTL	BD mode		
0	1	1	Differential Single Ended	1 × BTL +2 × SE	BD mode, BTL Differential		
1	0	0	Single Ended	4 × SE	AD mode		
1	0	1	Differential	1 × PBTL	INPUT_C ⁽¹⁾	INPUT_D ⁽¹⁾	
					0	0	AD mode
					1	0	BD mode
1	1	0	Reserved				
1	1	1					

(1) INPUT_C and D are used to select between a subset of AD and BD mode operations in PBTL mode (1=VREG and 0=GND).

PACKAGE HEAT DISSIPATION RATINGS⁽¹⁾

PARAMETER	TAS5611PHD	TAS5611DKD
$R_{\theta JC}$ (°C/W) – 2 BTL or 4 SE channels	3.2	2.1
$R_{\theta JC}$ (°C/W) – 1 BTL or 2 SE channel(s)	5.4	3.5
$R_{\theta JC}$ (°C/W) – 1 SE channel	7.9	5.1
Pad Area ⁽²⁾	64 mm ²	80 mm ²

(1) J_C is junction-to-case, CH is case-to-heat sink

(2) $R_{\theta CH}$ is an important consideration. Assume a 2-mil thickness of thermal grease with a thermal conductivity of 2.5 W/mK between the pad area and the heat sink and both channels active. The $R_{\theta CH}$ with this condition is 1.1°C/W for the PHD package and 0.44°C/W for the DKD package.

Table 1. ORDERING INFORMATION⁽¹⁾

T_A	PACKAGE	DESCRIPTION
0°C–70°C	TAS5611PHD	64 pin HTQFP
0°C–70°C	TAS5611DKD	44 pin PSOP3

(1) For the most current package and ordering information, see the Package Option Addendum at the end of this document, or see the TI website at www.ti.com.

ABSOLUTE MAXIMUM RATINGS

over operating free-air temperature range unless otherwise noted ⁽¹⁾

	VALUE	UNIT	
VDD to GND	–0.3 to 13.2	V	
GVDD to GND	–0.3 to 13.2	V	
PVDD_X to GND_X ⁽²⁾	–0.3 to 53	V	
OUT_X to GND_X ⁽²⁾	–0.3 to 53	V	
BST_X to GND_X ⁽²⁾	–0.3 to 66.2	V	
BST_X to GVDD_X ⁽²⁾	–0.3 to 53	V	
VREG to GND	–0.3 to 4.2	V	
GND_X to GND	–0.3 to 0.3	V	
GND to AGND	–0.3 to 0.3	V	
OC_ADJ, M1, M2, M3, OSC_IO+, OSC_IO-, FREQ_ADJ, VI_CM, C_STARTUP, PSU_REF to GND	–0.3 to 4.2	V	
INPUT_X	–0.3 to 7	V	
RESET, SD, OTW1, OTW2, CLIP, READY to GND	–0.3 to 7	V	
Continuous sink current (SD, OTW1, OTW2, CLIP, READY)	9	mA	
Operating junction temperature range, T _J	0 to 150	°C	
Storage temperature, T _{stg}	–40 to 150	°C	
Electrostatic discharge	Human body model ⁽³⁾ (all pins)	±2	kV
	Charged device model ⁽³⁾ (all pins)	±500	V

- (1) Stresses beyond those listed under *Absolute Maximum Ratings* may cause permanent damage to the device. These are stress ratings only, and functional operation of the device at these or any other conditions beyond those indicated under *Recommended Operating Conditions* is not implied. Exposure to absolute-maximum-rated conditions for extended periods may affect device reliability.
- (2) These voltages represents the DC voltage + peak AC waveform measured at the terminal of the device in all conditions.
- (3) Failure to follow good anti-static ESD handling during manufacture and rework will contribute to device malfunction. Please ensure operators handling the device are adequately grounded through the use of ground straps or alternative ESD protection.

RECOMMENDED OPERATING CONDITIONS

over operating free-air temperature range (unless otherwise noted)

			MIN	TYP	MAX	UNIT
PVDD_x	Half-bridge supply	DC supply voltage	16	32.5	34.1	V
GVDD_x	Supply for logic regulators and gate-drive circuitry	DC supply voltage	10.8	12	13.2	V
VDD	Digital regulator supply voltage	DC supply voltage	10.8	12	13.2	V
R _L (BTL)	Load impedance	Output filter according to schematics in the application information section	3.5	4		Ω
R _L (SE)			1.8	2		
R _L (PBTL)			1.6	2		
R _L (BTL)	Load impedance	Output filter according to schematics in the application information section and add Schottky diodes on all output nodes to GND_X, ROC = 22kΩ	2.8	3		Ω
L _{OUTPUT} (BTL)	Output filter inductance	Minimum output inductance at I _{OC}	7	10		μH
L _{OUTPUT} (SE)			7	15		
L _{OUTPUT} (PBTL)			7	10		
F _{PWM}	PWM frame rate selectable for AM interference avoidance; 1% Resistor tolerance.	Nominal	350	400	450	kHz
		AM1	300	340	380	
		AM2	260	300	335	
R _{FREQ_ADJ}	PWM frame rate programming resistor	Nominal; Master mode	9.5	10	10.5	kΩ
		AM1; Master mode	19.8	20	20.2	
		AM2; Master mode	29.7	30	30.3	
C _{PVDD}	PVDD close decoupling capacitors		2.0		μF	
R _{OC}	Over-current programming resistor	Resistor tolerance = 5%	22	30		kΩ
R _{OC_LATCHED}	Over-current programming resistor	Resistor tolerance = 5%	47	64		kΩ

RECOMMENDED OPERATING CONDITIONS (continued)

over operating free-air temperature range (unless otherwise noted)

		MIN	TYP	MAX	UNIT
$V_{\text{FREQ_ADJ}}$	Voltage on FREQ_ADJ pin for slave mode operation		3.3		V
		Slave mode			
T_J	Junction temperature	0		150	°C

PIN FUNCTIONS

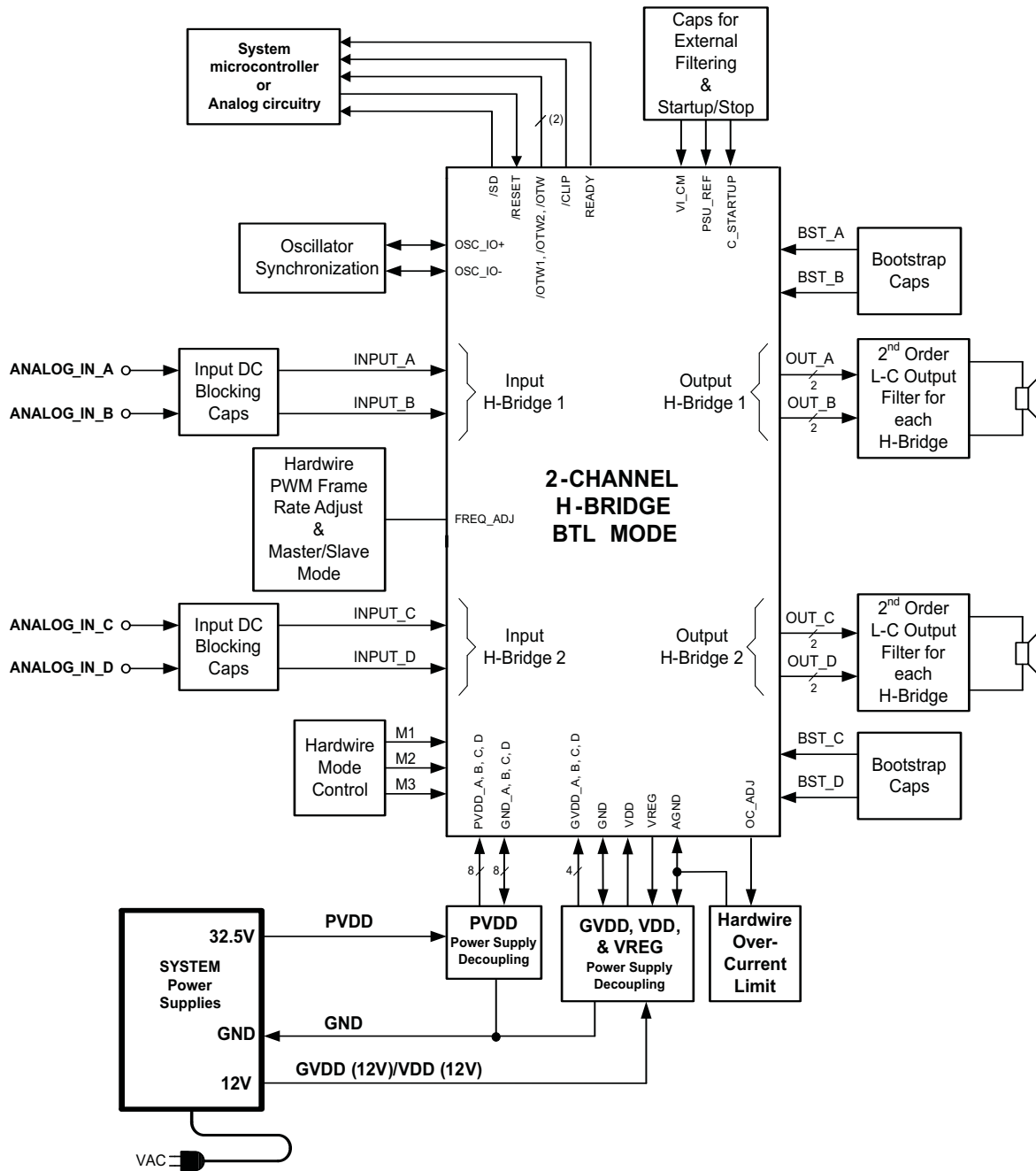
PIN			FUNCTION ⁽¹⁾	DESCRIPTION
NAME	PHD NO.	DKD NO.		
AGND	8	10	P	Analog ground
BST_A	54	43	P	HS bootstrap supply (BST), external 0.033 μ F capacitor to OUT_A required.
BST_B	41	34	P	HS bootstrap supply (BST), external 0.033 μ F capacitor to OUT_B required.
BST_C	40	33	P	HS bootstrap supply (BST), external 0.033 μ F capacitor to OUT_C required.
BST_D	27	24	P	HS bootstrap supply (BST), external 0.033 μ F capacitor to OUT_D required.
$\overline{\text{CLIP}}$	18	—	O	Clipping warning; open drain; active low
C_STARTUP	3	5	O	Startup ramp requires a charging capacitor of 4.7 nF to GND in BTL mode
FREQ_ADJ	12	14	I	PWM frame rate programming pin requires resistor to GND
GND	7, 23, 24, 57, 58	9	P	Ground
GND_A	48, 49	38	P	Power ground for half-bridge A
GND_B	46, 47	37	P	Power ground for half-bridge B
GND_C	34, 35	30	P	Power ground for half-bridge C
GND_D	32, 33	29	P	Power ground for half-bridge D
GVDD_A	55	—	P	Gate drive voltage supply requires 0.1 μ F capacitor to GND_A
GVDD_B	56	—	P	Gate drive voltage supply requires 0.1 μ F capacitor to GND_B
GVDD_C	25	—	P	Gate drive voltage supply requires 0.1 μ F capacitor to GND_C
GVDD_D	26	—	P	Gate drive voltage supply requires 0.1 μ F capacitor to GND_D
GVDD_AB	—	44	P	Gate drive voltage supply requires 0.22 μ F capacitor to GND_A/GND_B
GVDD_CD	—	23	P	Gate drive voltage supply requires 0.22 μ F capacitor to GND_C/GND_D
INPUT_A	4	6	I	Input signal for half bridge A
INPUT_B	5	7	I	Input signal for half bridge B
INPUT_C	10	12	I	Input signal for half bridge C
INPUT_D	11	13	I	Input signal for half bridge D
M1	20	20	I	Mode selection
M2	21	21	I	Mode selection
M3	22	22	I	Mode selection
NC	59–62	—	—	No connect, pins may be grounded.
OC_ADJ	1	3	O	Analog overcurrent programming pin requires 30k Ω resistor to GND.
OSC_IO+	13	15	I/O	Oscillator master/slave output/input.
OSC_IO–	14	16	I/O	Oscillator master/slave output/input.
$\overline{\text{OTW}}$	—	18	O	Overtemperature warning signal, open drain, active low.
$\overline{\text{OTW1}}$	16	—	O	Overtemperature warning signal, open drain, active low.
$\overline{\text{OTW2}}$	17	—	O	Overtemperature warning signal, open drain, active low.
OUT_A	52, 53	39, 40	O	Output, half bridge A
OUT_B	44, 45	36	O	Output, half bridge B
OUT_C	36, 37	31	O	Output, half bridge C
OUT_D	28, 29	27, 28	O	Output, half bridge D
PSU_REF	63	1	P	PSU Reference requires close decoupling of 330 pF to GND
PVDD_A	50, 51	41, 42	P	Power supply input for half bridge A requires close decoupling of 2 μ F capacitor GND_A
PVDD_B	42, 43	35	P	Power supply input for half bridge B requires close decoupling of 2 μ F capacitor GND_B
PVDD_C	38, 39	32	P	Power supply input for half bridge C requires close decoupling of 2 μ F capacitor GND_C
PVDD_D	30, 31	25, 26	P	Power supply input for half bridge D requires close decoupling of 2 μ F capacitor GND_D

(1) I = Input, O = Output, P = Power

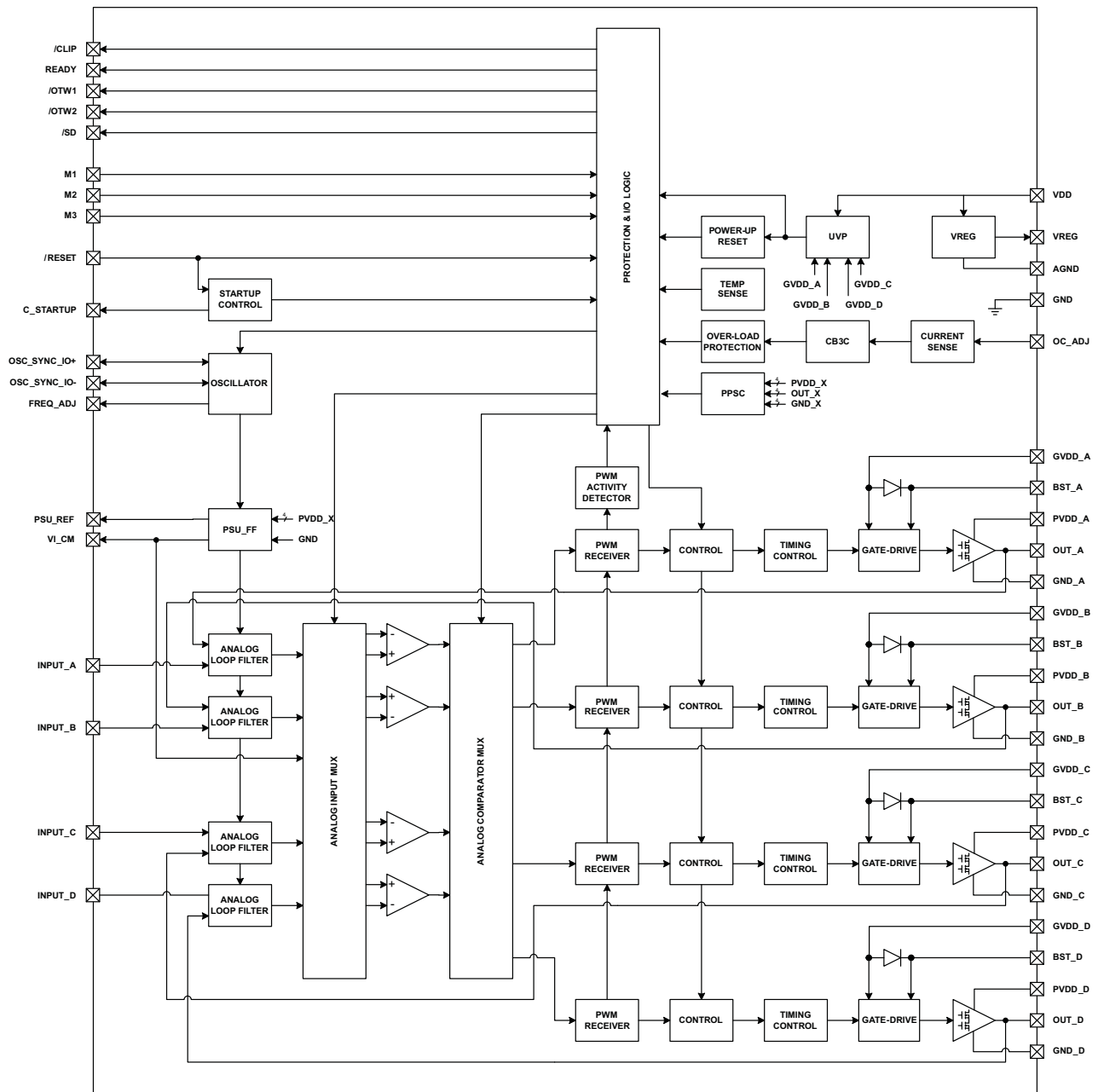
PIN FUNCTIONS (continued)

PIN			FUNCTION ⁽¹⁾	DESCRIPTION
NAME	PHD NO.	DKD NO.		
READY	19	19	O	Normal operation; open drain; active high
$\overline{\text{RESET}}$	2	4	I	Device reset Input; active low
$\overline{\text{SD}}$	15	17	O	Shutdown signal, open drain, active low
VDD	64	2	P	Power supply for digital voltage regulator requires a 10- μF capacitor in parallel with a 0.1- μF capacitor to GND for decoupling.
VI_CM	6	8	O	Analog comparator reference node requires close decoupling of 1nF to GND
VREG	9	11	P	Digital regulator supply filter pin requires 0.1- μF capacitor to GND

TYPICAL SYSTEM BLOCK DIAGRAM



FUNCTIONAL BLOCK DIAGRAM



AUDIO CHARACTERISTICS (BTL)

PCB and system configuration are in accordance with recommended guidelines. Audio frequency = 1kHz, PVDD_X = 32.5V, GVDD_X = 12 V, $R_L = 4\Omega$, $f_S = 400\text{kHz}$, $R_{OC} = 30\text{k}\Omega$, $T_C = 75^\circ\text{C}$, Output Filter: $L_{DEM} = 7\mu\text{H}$, $C_{DEM} = 680\text{nF}$, MODE = 010, unless otherwise noted.

PARAMETER		TEST CONDITIONS	MIN	TYP	MAX	UNIT
P _O	Power output per channel	R _L = 3 Ω, 10% THD+N (add Schottky diodes on all output nodes OUT_X to GND_X, ROC = 22kΩ)		165		W
		R _L = 4 Ω, 10% THD+N		125		
		R _L = 3 Ω, 1% THD+N (add Schottky diodes on all output nodes OUT_X to GND_X, ROC = 22kΩ)		130		
		R _L = 4 Ω, 1% THD+N		105		
THD+N	Total harmonic distortion + noise	1 W		0.03		%
V _n	Output integrated noise	A-weighted, AES17 filter, Input Capacitor Grounded		168		μV
V _{OS}	Output offset voltage	Inputs AC coupled to GND		20	40	mV
SNR	Signal-to-noise ratio ⁽¹⁾	A-weighted, AES17 filter		100		dB
DNR	Dynamic range	A-weighted, AES17 filter		100		dB
P _{idle}	Power dissipation due to Idle losses (I _{PVDD_X})	P _O = 0, 4 channels switching ⁽²⁾		1.3		W

(1) SNR is calculated relative to 1% THD+N output level..

(2) Actual system idle losses also are affected by core losses of output inductors.

AUDIO CHARACTERISTICS (PBTL)

PCB and system configuration are in accordance with recommended guidelines. Audio frequency = 1kHz, PVDD_X = 32.5V, GVDD_X = 12 V, $R_L = 2\Omega$, $f_S = 400\text{kHz}$, $R_{OC} = 30\text{k}\Omega$, $T_C = 75^\circ\text{C}$, Output Filter: $L_{DEM} = 7\mu\text{H}$, $C_{DEM} = 1.5\mu\text{F}$, MODE = 101-10, unless otherwise noted.

PARAMETER		TEST CONDITIONS	MIN	TYP	MAX	UNIT
P _O	Power output per channel	R _L = 2 Ω, 10% THD+N		250		W
		R _L = 3 Ω, 10% THD+N		165		
		R _L = 4 Ω, 10% THD+N		125		
		R _L = 2 Ω, 1% THD+N		210		
		R _L = 3 Ω, 1% THD+N		135		
		R _L = 4 Ω, 1% THD+N		105		
THD+N	Total harmonic distortion + noise	1 W		0.03		%
V _n	Output integrated noise	A-weighted		170		μV
SNR	Signal to noise ratio ⁽¹⁾	A-weighted		100		dB
DNR	Dynamic range	A-weighted		100		dB
P _{idle}	Power dissipation due to idle losses (IPVDD_X)	P _O = 0, 4 channels switching ⁽²⁾		1.3		W

(1) SNR is calculated relative to 1% THD-N output level.

(2) Actual system idle losses are affected by core losses of output inductors.

ELECTRICAL CHARACTERISTICS

PVDD_X = 32.5V, GVDD_X = 12 V, VDD = 12 V, T_C (Case temperature) = 75°C, f_s = 400 kHz, unless otherwise specified.

PARAMETER		TEST CONDITIONS	MIN	TYP	MAX	UNIT
INTERNAL VOLTAGE REGULATOR AND CURRENT CONSUMPTION						
VREG	Voltage regulator, only used as reference node, VREG	VDD = 12 V	3	3.3	3.6	V
VI_CM	Analog comparator reference node, VI_CM		1.5	1.75	1.9	V
I _{VDD}	VDD supply current	Operating, 50% duty cycle	20			mA
		Idle, reset mode	20			
I _{GVDD_X}	GVDD_x gate-supply current per half-bridge	50% duty cycle	10			mA
		Reset mode	1.5			
I _{PVDD_X}	Half-bridge supply current	50% duty cycle with recommended output filter	10			mA
		Reset mode, No switching	540			
ANALOG INPUTS						
R _{IN}	Input resistance	READY = HIGH	33			kΩ
V _{IN}	Maximum input voltage swing		7			V
I _{IN}	Maximum input current		1			mA
G	Voltage Gain (V _{OUT} /V _{IN})		21			dB
OSCILLATOR						
f _{OSC_IO+}	Nominal, Master Mode	F _{PWM} × 10	3.5	4	4.5	MHz
	AM1, Master Mode		3.0	3.4	3.8	
	AM2, Master Mode		2.6	3	3.35	
V _{IH}	High level input voltage		1.86			V
V _{IL}	Low level input voltage		1.45			V
OUTPUT-STAGE MOSFETS						
R _{DS(on)}	Drain-to-source resistance, low side (LS)	T _J = 25°C, excludes metallization resistance, GVDD = 12 V	60	100	mΩ	
	Drain-to-source resistance, high side (HS)		60	100	mΩ	

ELECTRICAL CHARACTERISTICS (continued)

PVDD_X = 32.5V, GVDD_X = 12 V, VDD = 12 V, T_C (Case temperature) = 75°C, f_s = 400 kHz, unless otherwise specified.

PARAMETER		TEST CONDITIONS	MIN	TYP	MAX	UNIT
I/O PROTECTION						
V _{uvp,G}	Undervoltage protection limit, GVDD_x and VDD			9.5		V
V _{uvp,hyst} ⁽¹⁾				0.6		V
OTW1 ⁽¹⁾	Overtemperature warning 1		95	100	105	°C
OTW2 ⁽¹⁾	Overtemperature warning 2		115	125	135	°C
OTW _{hyst} ⁽¹⁾	Temperature drop needed below OTW temperature for OTW to be inactive after OTW event.			25		°C
OTE ⁽¹⁾	Overtemperature error		145	155	165	°C
	OTE-OTW differential			30		°C
OTE _{hyst} ⁽¹⁾	A reset needs to occur for \overline{SD} to be released following an OTE event			25		°C
OLPC	Overload protection counter	f _{PWM} = 400 kHz		2.6		ms
I _{OC}	Overcurrent limit protection	Resistor – programmable, nominal peak current in 1Ω load, R _{OCP} = 30kΩ		12.6		A
		Resistor – programmable, nominal peak current in 1Ω load, R _{OCP} = 22kΩ (add Schottky diodes on all output nodes OUT_X to GND_X)		16.3		A
I _{OC_LATCHED}	Overcurrent limit protection	Resistor – programmable, nominal peak current in 1Ω load, R _{OCP} = 64kΩ		12.6		A
		Resistor – programmable, nominal peak current in 1Ω load, R _{OCP} = 47kΩ (add Schottky diodes on all output nodes OUT_X to GND_X)		16.3		A
I _{OCT}	Overcurrent response time	Time from switching transition to flip-state induced by overcurrent		150		ns
I _{PD}	Internal pulldown resistor at output of each half bridge	Connected when \overline{RESET} is active to provide bootstrap charge. Not used in SE mode.		3		mA
STATIC DIGITAL SPECIFICATIONS						
V _{IH}	High level input voltage	INPUT_X, M1, M2, M3, RESET	1.9			V
V _{IL}	Low level input voltage			0.8		V
I _{lkg}	Input leakage current			100		μA
OTW/SHUTDOWN (SD)						
R _{INT_PU}	Internal pullup resistance, $\overline{OTW1}$ to VREG, $\overline{OTW2}$ to VREG, \overline{SD} to VREG		20	26	32	kΩ
V _{OH}	High level output voltage	Internal pullup resistor	3	3.3	3.6	V
		External pullup of 4.7 kΩ to 5 V	4.5		5	
V _{OL}	Low level output voltage	I _O = 4 mA		200	500	mV
FANOUT	Device fanout $\overline{OTW1}$, $\overline{OTW2}$, \overline{SD} , \overline{CLIP} , \overline{READY}	No external pullup		30		devices

(1) Specified by design.

TYPICAL CHARACTERISTICS, BTL CONFIGURATION

TOTAL HARMONIC+NOISE vs OUTPUT POWER

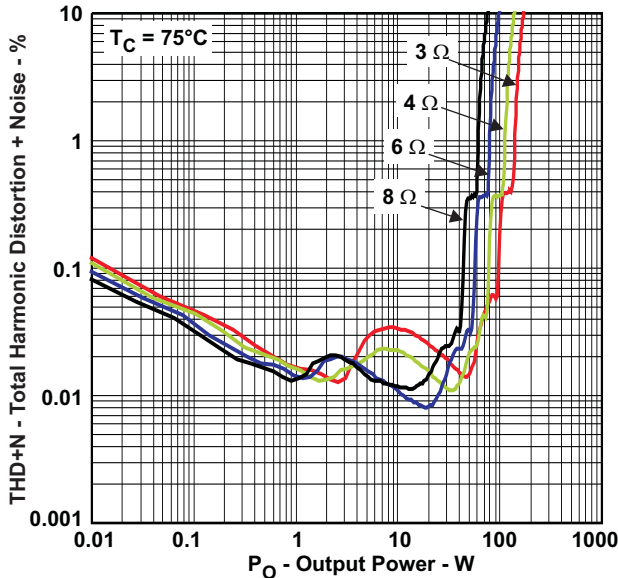


Figure 1.

OUTPUT POWER vs SUPPLY VOLTAGE

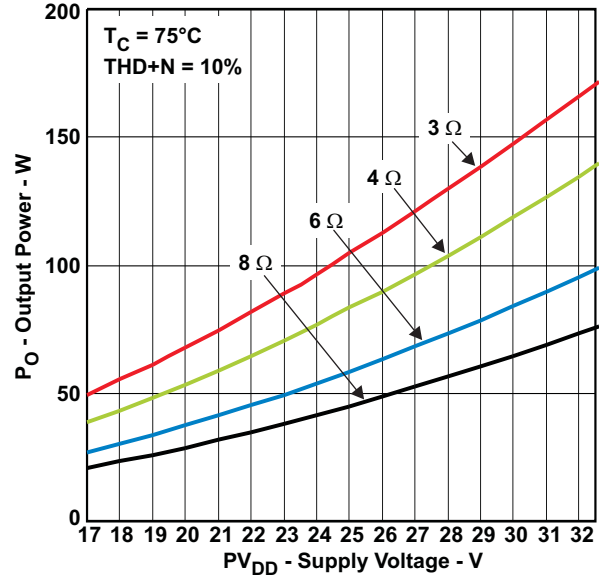


Figure 2.

UNCLIPPED OUTPUT POWER vs SUPPLY VOLTAGE

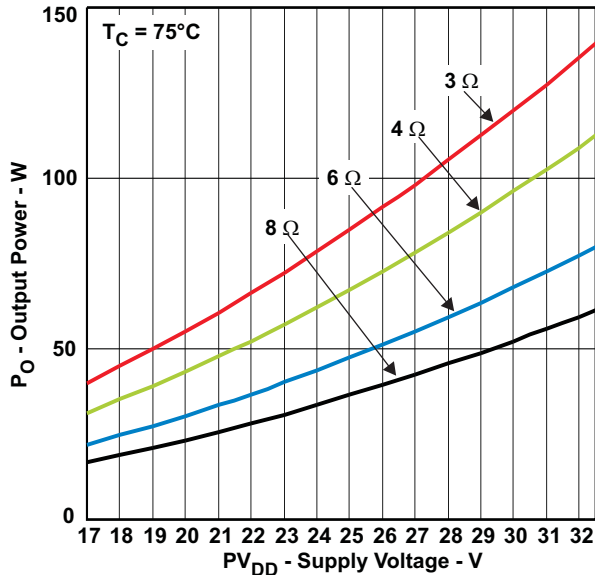


Figure 3.

SYSTEM EFFICIENCY vs OUTPUT POWER

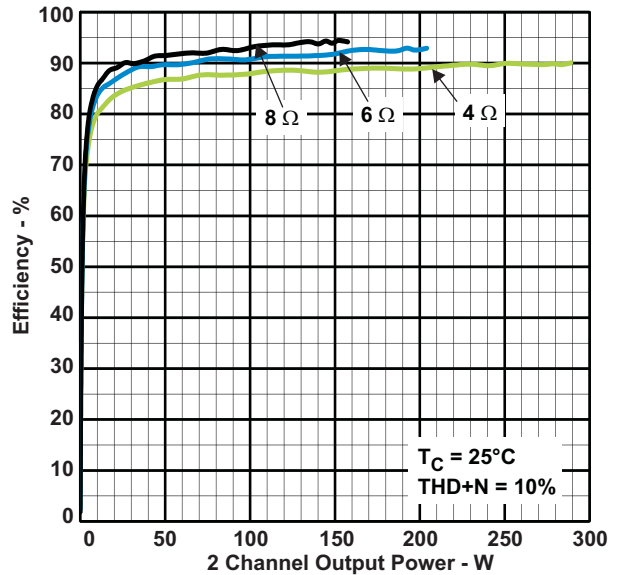


Figure 4.

TYPICAL CHARACTERISTICS, BTL CONFIGURATION (continued)

**SYSTEM POWER LOSS
VS
OUTPUT POWER**

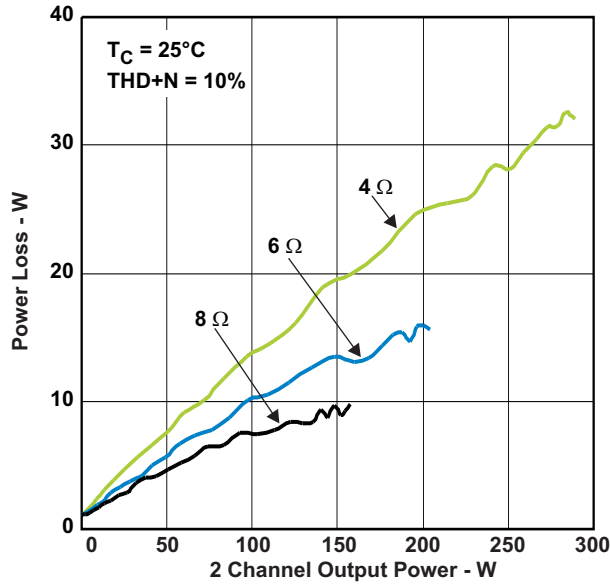


Figure 5.

**OUTPUT POWER
VS
CASE TEMPERATURE**

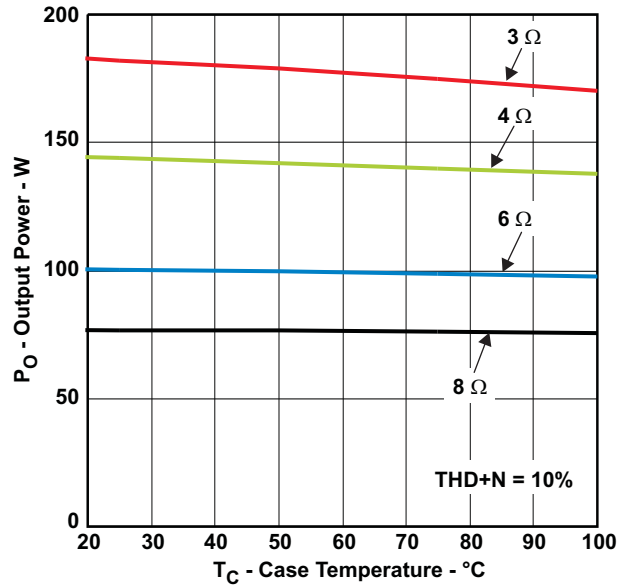


Figure 6.

**NOISE AMPLITUDE
VS
FREQUENCY**

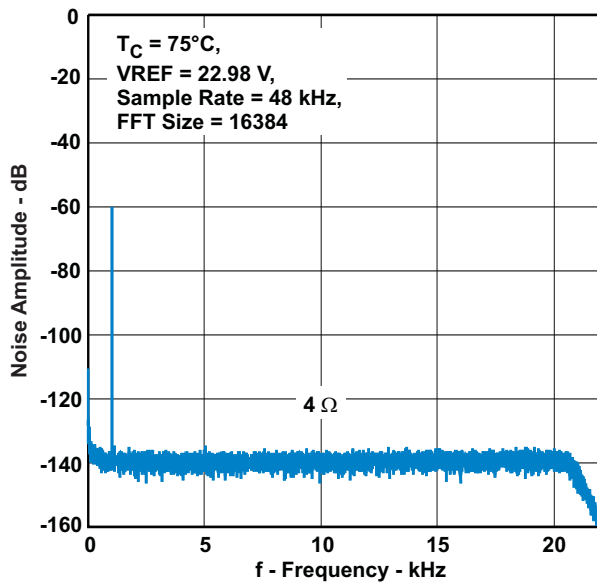


Figure 7.

**TOTAL HARMONIC DISTORTION+NOISE
VS
FREQUENCY**

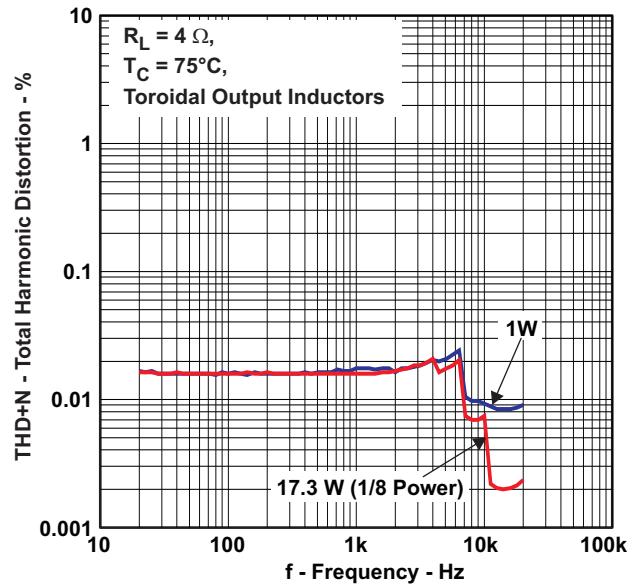


Figure 8.

TYPICAL CHARACTERISTICS, PBTL CONFIGURATION

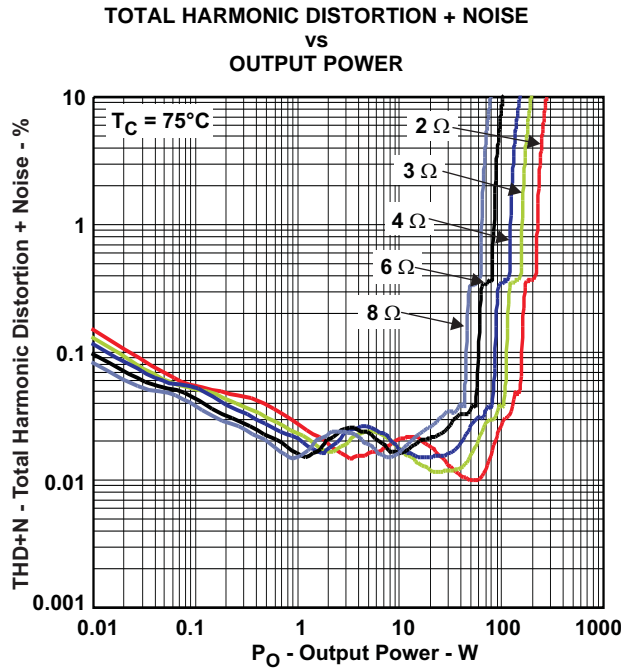


Figure 9.

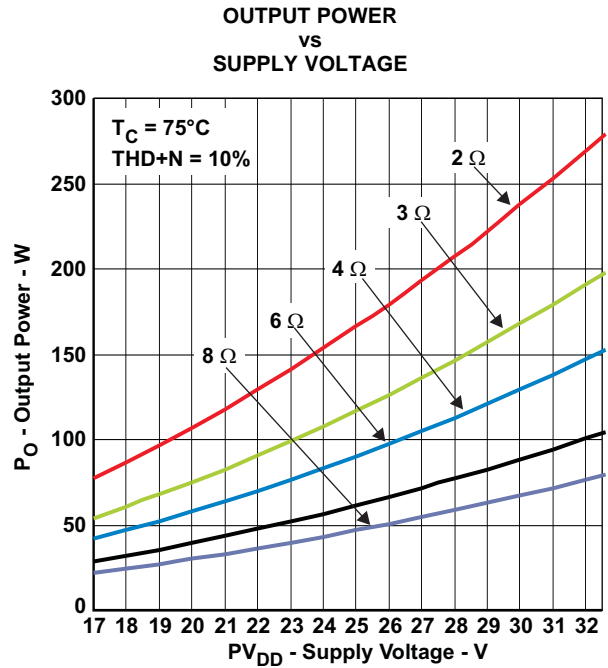


Figure 10.

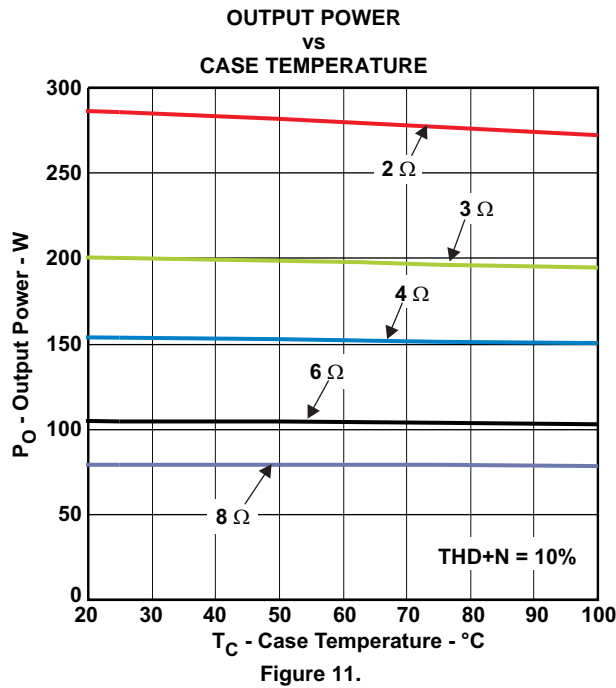


Figure 11.

APPLICATION INFORMATION

PCB MATERIAL RECOMMENDATION

FR-4 Glass Epoxy material with 2 oz. (70 μ m) is recommended for use with the TAS5611. The use of this material can provide for higher power output, improved thermal performance, and better EMI margin (due to lower PCB trace inductance).

PVDD CAPACITOR RECOMMENDATION

The large capacitors used in conjunction with each full-bridge, are referred to as the PVDD Capacitors. These capacitors should be selected for proper voltage margin and adequate capacitance to support the power requirements. In practice, with a well designed system power supply, 1000 μ F, 50V will support more applications. The PVDD capacitors should be low ESR type because they are used in a circuit associated with high-speed switching.

DECOUPLING CAPACITOR RECOMMENDATIONS

To design an amplifier that has robust performance, passes regulatory requirements, and exhibits good audio performance, a quality decoupling capacitors should be used. In practice, X7R should be used in this application.

The voltage of the decoupling capacitors should be selected in accordance with good design practices. Temperature, ripple current, and voltage overshoot must be considered. This fact is particularly true in the selection of the 2 μ F that is placed on the power supply to each half-bridge. It must withstand the voltage overshoot of the PWM switching, the heat generated by the amplifier during high power output, and the ripple current created by high power output. A minimum voltage rating of 50V is required for use with a 32.5V power supply.

SYSTEM DESIGN RECOMMENDATIONS

The following schematics and PCB layouts illustrate *best practices* used for the TAS5611.

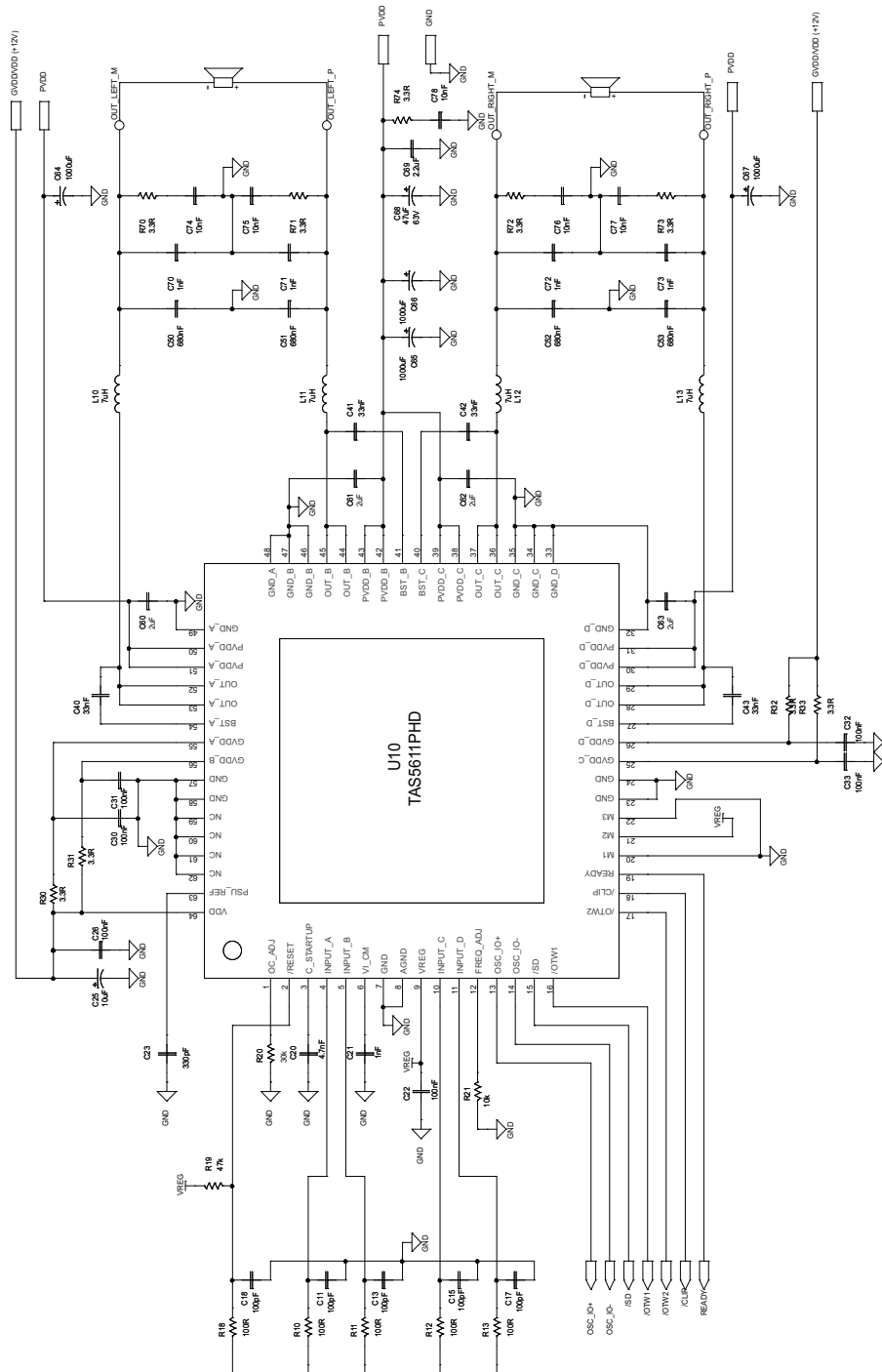


Figure 12. Typical Differential Input BTL Application With BD Modulation Filters

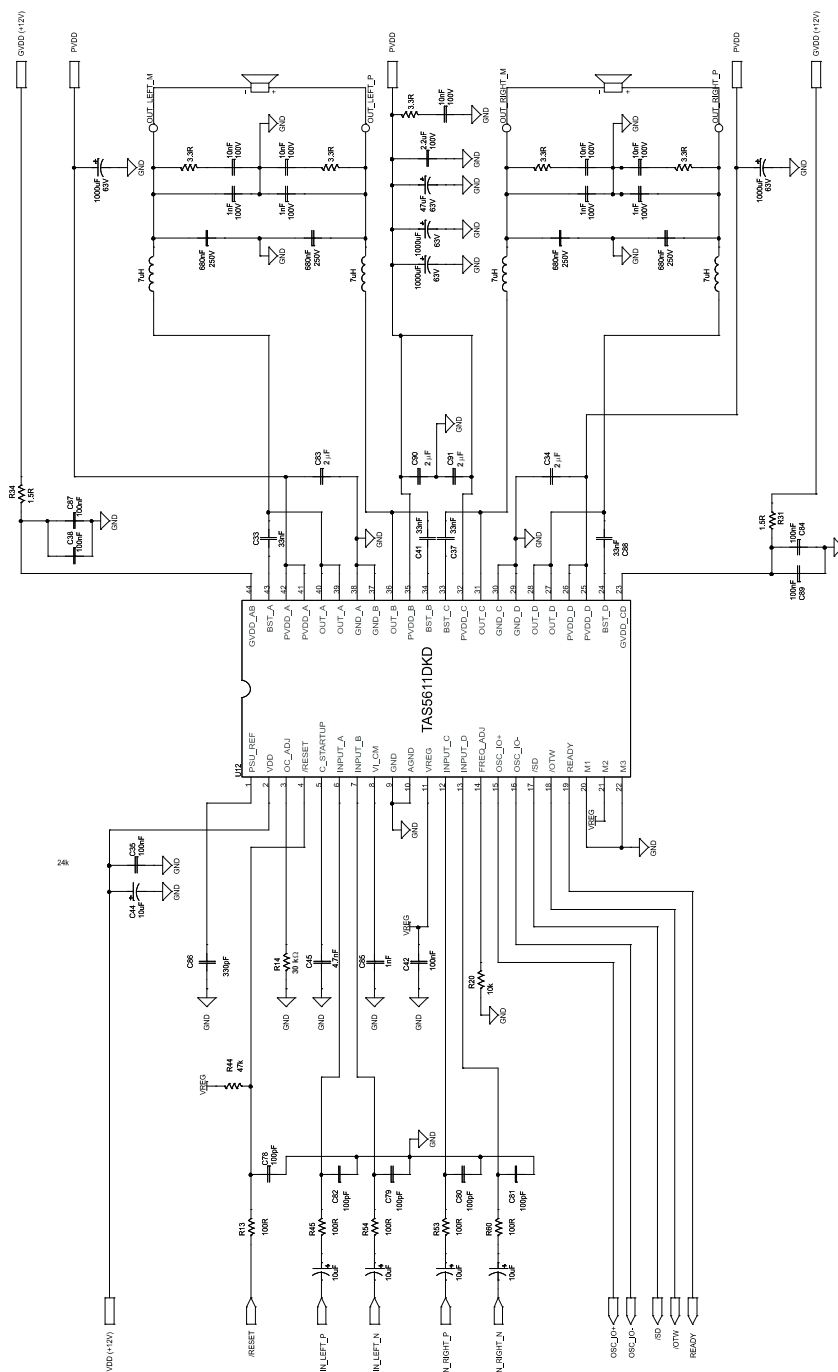


Figure 14. Typical Differential Input BTL Application With BD Modulation Filters DKD Package

THEORY OF OPERATION

POWER SUPPLIES

To facilitate system design, the TAS5611 needs only a 12V supply in addition to the (typical) 32.5V power-stage supply. An internal voltage regulator provides suitable voltage levels for the digital and low-voltage analog circuitry. Additionally, all circuitry requiring a floating voltage supply, e.g., the high-side gate drive, is accommodated by built-in bootstrap circuitry requiring only an external capacitor for each half-bridge.

To provide outstanding electrical and acoustical characteristics, the PWM signal path including gate drive and output stage is designed as identical, independent half-bridges. For this reason, each half-bridge has separate gate drive supply (GVDD_X), bootstrap pins (BST_X), and power-stage supply pins (PVDD_X). Furthermore, an additional pin (VDD) is provided as supply for all common circuits. Although supplied from the same 12V source, it is highly recommended to separate GVDD_A, GVDD_B, GVDD_C, GVDD_D, and VDD on the printed-circuit board (PCB) by RC filters (see application diagram for details). These RC filters provide the recommended high-frequency isolation. Special attention should be paid to placing all decoupling capacitors as close to their associated pins as possible. In general, inductance between the power supply pins and decoupling capacitors must be avoided. (See reference board documentation for additional information.)

For a properly functioning bootstrap circuit, a small ceramic capacitor must be connected from each bootstrap pin (BST_X) to the power-stage output pin (OUT_X). When the power-stage output is low, the bootstrap capacitor is charged through an internal diode connected between the gate-drive power-supply pin (GVDD_X) and the bootstrap pin. When the powerstage output is high, the bootstrap capacitor potential is shifted above the output potential and thus provides a suitable voltage supply for the high-side gate driver. In an application with PWM switching frequencies in the range from 300kHz to 400kHz, it is recommended to use 33nF ceramic capacitors, size 0603 or 0805, for the bootstrap supply. These 33nF capacitors ensure sufficient energy storage, even during minimal PWM duty cycles, to keep the high-side power stage FET (LDMOS) fully turned on during the remaining part of the PWM cycle.

Special attention should be paid to the power-stage power supply; this includes component selection, PCB placement, and routing. As indicated, each half-bridge has independent power-stage supply pins (PVDD_X). For optimal electrical performance, EMI compliance, and system reliability, it is important that each PVDD_X pin is decoupled with a 2 μ F ceramic capacitor placed as close as possible to each supply pin. It is recommended to follow the PCB layout of the TAS5611 reference design. For additional information on recommended power supply and required components, see the application diagrams in this data sheet.

The 12V supply should be from a low-noise, low-output impedance voltage regulator. Likewise, the 32.5V power-stage supply is assumed to have low output impedance and low noise. The power-supply sequence is not critical as facilitated by the internal power-on-reset circuit. Moreover, the TAS5611 is fully protected against erroneous power-stage turn on due to parasitic gate charging. Thus, voltage-supply ramp rates (dV/dt) are non-critical within the specified range (see the [Recommended Operating Conditions](#) table of this data sheet).

SYSTEM POWER-UP/POWER-DOWN SEQUENCE

Powering Up

The TAS5611 does not require a power-up sequence. The outputs of the H-bridges remain in a high-impedance state until the gate-drive supply voltage (GVDD_X) and VDD voltage are above the undervoltage protection (UVP) voltage threshold (see the [Electrical Characteristics](#) table of this data sheet). Although not specifically required, it is recommended to hold $\overline{\text{RESET}}$ in a low state while powering up the device. This allows an internal circuit to charge the external bootstrap capacitors by enabling a weak pulldown of the half-bridge output.

Powering Down

The TAS5611 does not require a power-down sequence. The device remains fully operational as long as the gate-drive supply (GVDD_X) voltage and VDD voltage are above the undervoltage protection (UVP) voltage threshold (see the [Electrical Characteristics](#) table of this data sheet). Although not specifically required, it is a good practice to hold $\overline{\text{RESET}}$ low during power down, thus preventing audible artifacts including pops or clicks.

ERROR REPORTING

The \overline{SD} , \overline{OTW} , $\overline{OTW1}$ and $\overline{OTW2}$ pins are active low, open-drain outputs. Their function is for protection-mode signaling to a PWM controller or other system-control device.

Any fault resulting in device shutdown is signaled by the \overline{SD} pin going low. Likewise, \overline{OTW} and $\overline{OTW2}$ goes low when the device junction temperature exceeds 125°C and $\overline{OTW1}$ goes low when the junction temperature exceeds 100°C (see the following table).

\overline{SD}	$\overline{OTW1}$	$\overline{OTW2}$, \overline{OTW}	DESCRIPTION
0	0	0	Overtemperature (OTE) or overload (OLP) or undervoltage (UVP)
0	0	1	Overload (OLP) or undervoltage (UVP). Junction temperature higher than 100°C (overtemperature warning)
0	1	1	Overload (OLP) or undervoltage (UVP)
1	0	0	Junction temperature higher than 125°C (overtemperature warning)
1	0	1	Junction temperature higher than 100°C (overtemperature warning)
1	1	1	Junction temperature lower than 100°C and no OLP or UVP faults (normal operation)

Note that asserting either \overline{RESET} low forces the \overline{SD} signal high, independent of faults being present. TI recommends monitoring the \overline{OTW} signal using the system microcontroller and responding to an overtemperature warning signal by, e.g., turning down the volume to prevent further heating of the device resulting in device shutdown (OTE).

To reduce external component count, an internal pullup resistor to 3.3V is provided on both \overline{SD} and \overline{OTW} outputs. Level compliance for 5V logic can be obtained by adding external pullup resistors to 5V (see the [Electrical Characteristics](#) tablen of this data sheet for further specifications).

DEVICE PROTECTION SYSTEM

The TAS5611 contains advanced protection circuitry carefully designed to facilitate system integration and ease of use, as well as to safeguard the device from permanent failure due to a wide range of fault conditions such as short circuits, overload, overtemperature, and undervoltage. The TAS5611 responds to a fault by immediately setting the power stage in a high-impedance (Hi-Z) state and asserting the SD pin low. In situations other than overload and overtemperature error (OTE), the device automatically recovers when the fault condition has been removed, i.e., the supply voltage has increased.

The device will function on errors, as shown in the following table.

BTL Mode		PBTL Mode		SE Mode	
Local error in	Turns Off or in	Local error in	Turns Off or in	Local error in	Turns Off or in
A	A+B	A	A+B+C+D	A	A+B
B		B		B	
C	C+D	C		C	C+D
D		D		D	

Bootstrap UVP does not shutdown according to the table, it shuts down the respective halfbridge.

PIN-TO-PIN SHORT CIRCUIT PROTECTION (PPSC)

The PPSC detection system protects the device from permanent damage if a power output pin (OUT_X) is shorted to GND_X or PVDD_X. For comparison, the OC protection system detects an over current after the demodulation filter where PPSC detects shorts directly at the pin before the filter. PPSC detection is performed at startup i.e. when VDD is supplied, consequently a short to either GND_X or PVDD_X after system startup will not activate the PPSC detection system. When PPSC detection is activated by a short on the output, all half bridges are kept in a Hi-Z state until the short is removed, the device then continues the startup sequence and starts switching. The detection is controlled globally by a two step sequence. The first step ensures that there are no shorts from OUT_X to GND_X, the second step tests that there are no shorts from OUT_X to PVDD_X. The total duration of this process is roughly proportional to the capacitance of the output LC filter. The typical duration is

<15ms/μF. While the PPSC detection is in progress, \overline{SD} is kept low, and the device will not react to changes applied to the \overline{RESET} pins. If no shorts are present the PPSC detection passes, and \overline{SD} is released. A device reset will not start a new PPSC detection. PPSC detection is enabled in BTL and PBTL output configurations, the detection is not performed in SE mode. To make sure the PPSC detection system is not tripped, it is recommended not to insert resistive load to GND_X or PVDD_X.

OVERTEMPERATURE PROTECTION

The two different package options has individual overtemperature protection schemes.

PHD Package:

The TAS5611 PHD package option has a three-level temperature-protection system that asserts an active low warning signal ($\overline{OTW1}$) when the device junction temperature exceeds 100°C (typical), ($\overline{OTW2}$) when the device junction temperature exceeds 125°C (typical) and, if the device junction temperature exceeds 155°C (typical), the device is put into thermal shutdown, resulting in all half-bridge outputs being set in the high-impedance (Hi-Z) state and \overline{SD} being asserted low. OTE is latched in this case. To clear the OTE latch, \overline{RESET} must be asserted. Thereafter, the device resumes normal operation.

DKD Package:

The TAS5611 DKD package option has a two-level temperature-protection system that asserts an active low warning signal (\overline{OTW}) when the device junction temperature exceeds 125°C (typical) and, if the device junction temperature exceeds 155°C (typical), the device is put into thermal shutdown, resulting in all half-bridge outputs being set in the high-impedance (Hi-Z) state and \overline{SD} being asserted low. OTE is latched in this case. To clear the OTE latch, \overline{RESET} must be asserted. Thereafter, the device resumes normal operation.

UNDERVOLTAGE PROTECTION (UVP) AND POWER-ON RESET (POR)

The UVP and POR circuits of the TAS5611 fully protect the device in any power-up/down and brownout situation. While powering up, the POR circuit resets the overload circuit (OLP) and ensures that all circuits are fully operational when the GVDD_X and VDD supply voltages reach stated in the [Electrical Characteristics](#) table. Although GVDD_X and VDD are independently monitored, a supply voltage drop below the UVP threshold on any VDD or GVDD_X pin results in all half-bridge outputs immediately being set in the high-impedance (Hi-Z) state and \overline{SD} being asserted low. The device automatically resumes operation when all supply voltages have increased above the UVP threshold.

DEVICE RESET

When \overline{RESET} is asserted low, all power-stage FETs in the four half-bridges are forced into a high-impedance (Hi-Z) state.

In BTL modes, to accommodate bootstrap charging prior to switching start, asserting the reset input low enables weak pulldown of the half-bridge outputs. In the SE mode, the output is forced into a high impedance state when asserting the reset input low. Asserting reset input low removes any fault information to be signaled on the \overline{SD} output, i.e., \overline{SD} is forced high. A rising-edge transition on reset input allows the device to resume operation after an overload fault. To ensure thermal reliability, the rising edge of reset must occur no sooner than 4 ms after the falling edge of \overline{SD} .

SYSTEM DESIGN CONSIDERATION

A rising-edge transition on reset input allows the device to execute the startup sequence and starts switching.

Apply only audio when the state of \overline{READY} is high that will start and stop the amplifier without having audible artifacts that is heard in the output transducers. If an overcurrent protection event is introduced the \overline{READY} signal goes low, hence, filtering is needed if the signal is intended for audio muting in non microcontroller systems.

The CLIP signal is indicating that the output is approaching clipping. The signal can be used to either an audio volume decrease or intelligent power supply controlling a low and a high rail.

The device is inverting the audio signal from input to output.

The VREG pin is not recommended to be used as a voltage source for external circuitry.

OSCILLATOR

The oscillator frequency can be trimmed by external control of the `FREQ_ADJ` pin.

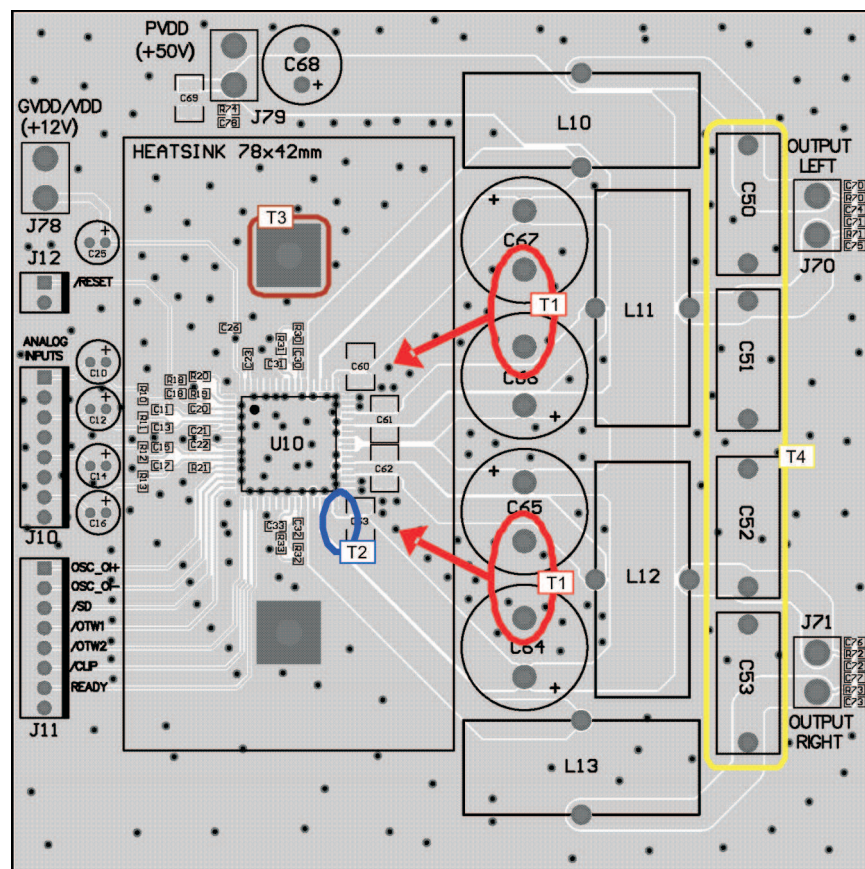
To reduce interference problems while using radio receiver tuned within the AM band, the switching frequency can be changed from nominal to lower values. These values should be chosen such that the nominal and the lower value switching frequencies together results in the fewest cases of interference throughout the AM band, and can be selected by the value of the `FREQ_ADJ` resistor connected to GND in master mode.

For slave mode operation, turn of the oscillator by pulling the `FREQ_ADJ` pin to VREG. This will configure the `OSC_I/O` pins as inputs and needs to be slaved from an external clock.

PRINTED CIRCUIT BOARD RECOMMENDATION

Use an unbroken ground plane to have good low impedance and inductance return path to the power supply for power and audio signals. PCB layout, audio performance and EMI are linked closely together. The circuit contains high fast switching currents; therefore, care must be taken to prevent damaging voltage spikes. Routing the audio input should be kept short and together with the accompanied audio source ground. A local ground area underneath the device is important to keep solid to minimize ground bounce.

Netlist for this printed circuit board is generated from the schematic in [Figure 12](#).



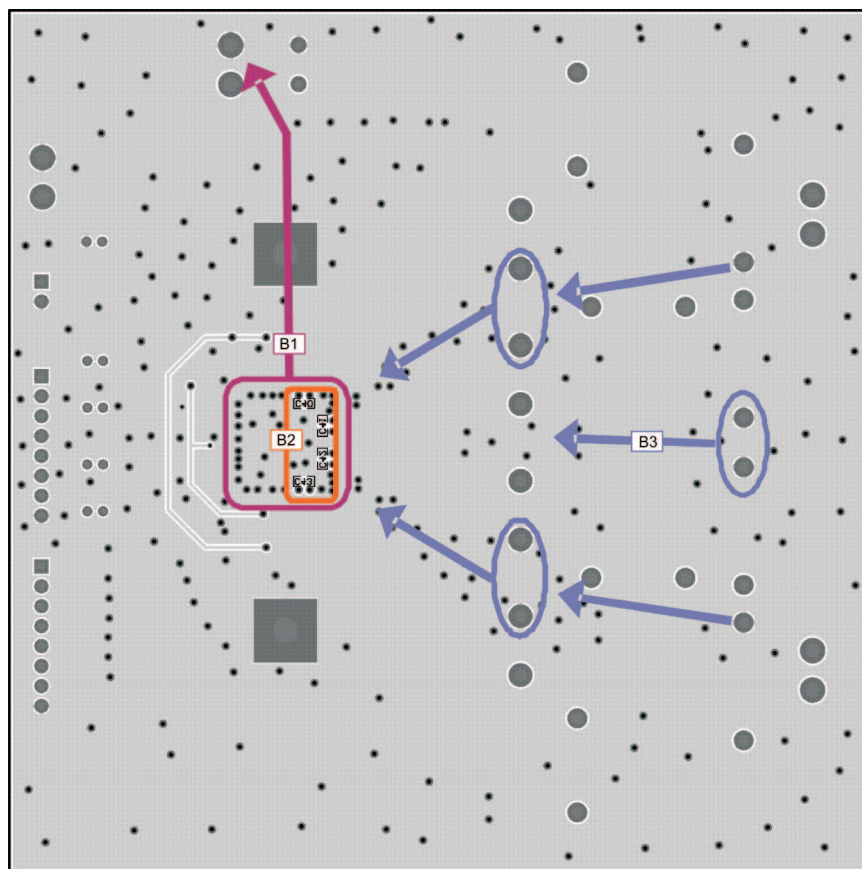
Note T1: PVDD decoupling bulk capacitors C60-C64 should be as close as possible to the PVDD and GND_X pins, the heat sink sets the distance. Wide traces should be routed on the top layer with direct connection to the pins and without going through vias. No vias or traces should be blocking the current path.

Note T2: Close decoupling of PVDD with low impedance X7R ceramic capacitors is placed under the heat sink and close to the pins.

Note T3: Heat sink needs to have a good connection to PCB ground.

Note T4: Output filter capacitors must be linear in the applied voltage range preferable metal film types.

Figure 15. Printed Circuit Board - Top Layer



Note B1: It is important to have a direct low impedance return path for high current back to the power supply. Keep impedance low from top to bottom side of PCB through a lot of ground vias.

Note B2: Bootstrap low impedance X7R ceramic capacitors placed on bottom side providing a short low inductance current loop.

Note B3: Return currents from bulk capacitors and output filter capacitors.

Figure 16. Printed Circuit Board - Bottom Layer

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